

# Numerical Calculation of a **2.8 kJ** Plasma Focus Characteristics Using a Five Phase Model

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# Abstract

- A radiative five-phase model for plasma focus (S. Lee model) (axial phase, inward radial phase, reflected shock phase, pinch phase and expanded phase) was applied to a 2.8 kJ plasma focus device to find the plasma parameters and the SXR radiation emitted from the plasma pinch at different gas pressures.
- Fitting the model parameters, the calculated and measured current waveforms at 0.75 Torr of Argon were obtained and compared.
- The results were tabulated for the optimal operating conditions and compared with the same features of other different PF devices (NX2, PF1000, PF400, and DPF78).

# Introduction

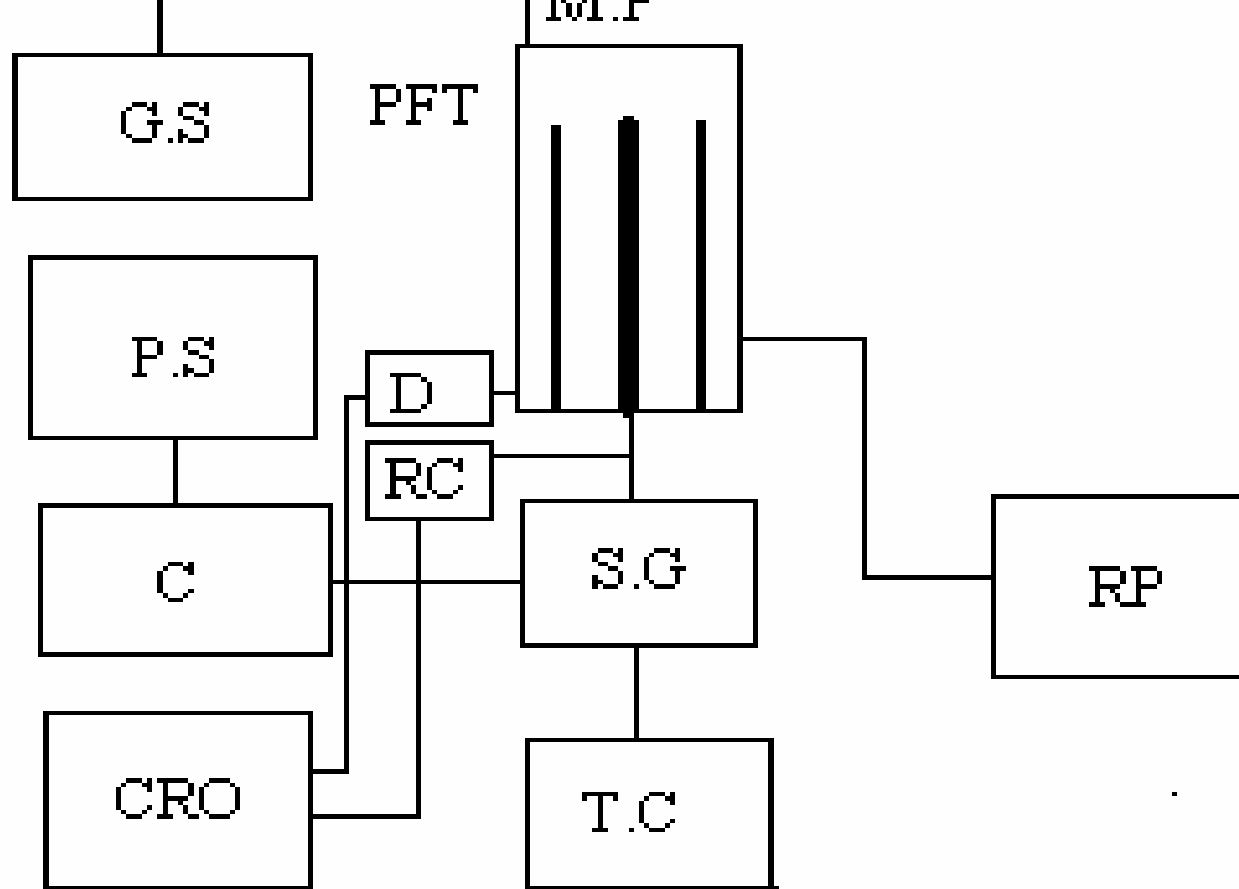
- As known, the plasma focus is generated by applying a high-pulse voltage to a low-pressure gas between two coaxial electrodes, with a high energy density, intense beams of charged particles and radiation emission including **SXR radiation**, which could be used in radiography and microelectronics lithography.
- In the early stage of Mather type - PF devices, a simple three phase model was developed to characterize their work, using a snow plow model in the axial phase and a slug model in the radial phase. Then, the model was modified to get a five phase model, in which the radial phase is divided into three radial sub-phases in addition to two essential phases (axial, and expanded). The sub-phases are a radial inward shock phase, a radial reflected shock phase and a slow compression (radiative) phase.

- This model is valid for many applications such as: the design of a cascading plasma focus; for estimating soft x-ray yield and for the purpose of developing a soft x-ray source (SXR) for microelectronics lithography.

- **The aim of this work** is to use the visual basic program written on the base of S Lee five phase radiative model distributed during the last **internet workshop on numerical plasma focus experiments to characterise our plasma focus device**, in comparison with other PF devices.

# Experimental setup

- Energy from the charger with specifications of 0-20 kV and 0-100 mA is stored in a 25 $\mu$ F, 20kV capacitor which is charged to 15 kV and switched by means of a spark gap which is in turn switched by a high voltage negative pulse getting from TV transformer of a triggering unit.
- The system is pumped down to a base pressure of 0.25 mbar and operated at pressures up to 5 mbar. The focus action is characterized by a distinctive dip in the current signal and a spike in the voltage signal, which indicate a rapid magnetic compression. an Ohmic voltage divider 1:100 and Rogowski coil were used to determine the voltage and current signals vs. the time during the plasma focus process using a storage oscilloscope with 1:10 attenuator.



**PF-Sy1 device:** PFT plasma focus tube, GS gas supplier, PS power supply, C bank capacitors, SG spark gap, TC triggering circuit, CRO storage oscilloscope, RP rotary pump, D voltage divider, RC Rogowski coil.

On the base of measured or calculated current waveform in the **case of a short circuit** , the parameters such: period **T** , inductance **L<sub>0</sub>**, resistance **r<sub>0</sub>** and the maximum current **I<sub>0</sub>** after the determining factor **f** could be found using the following formulae:

$$f = \frac{1}{n} \sum_n I_{n+1} / I_n$$

$$L_0 = T^2 / (4 \pi^2 C_0)$$

$$I_0 = \pi C_0 V_0 (1 + f) / T$$

$$r_0 = -\frac{2}{\pi} \ln(f) (L_0 / C_0)^{1/2}$$

# Results and discussion

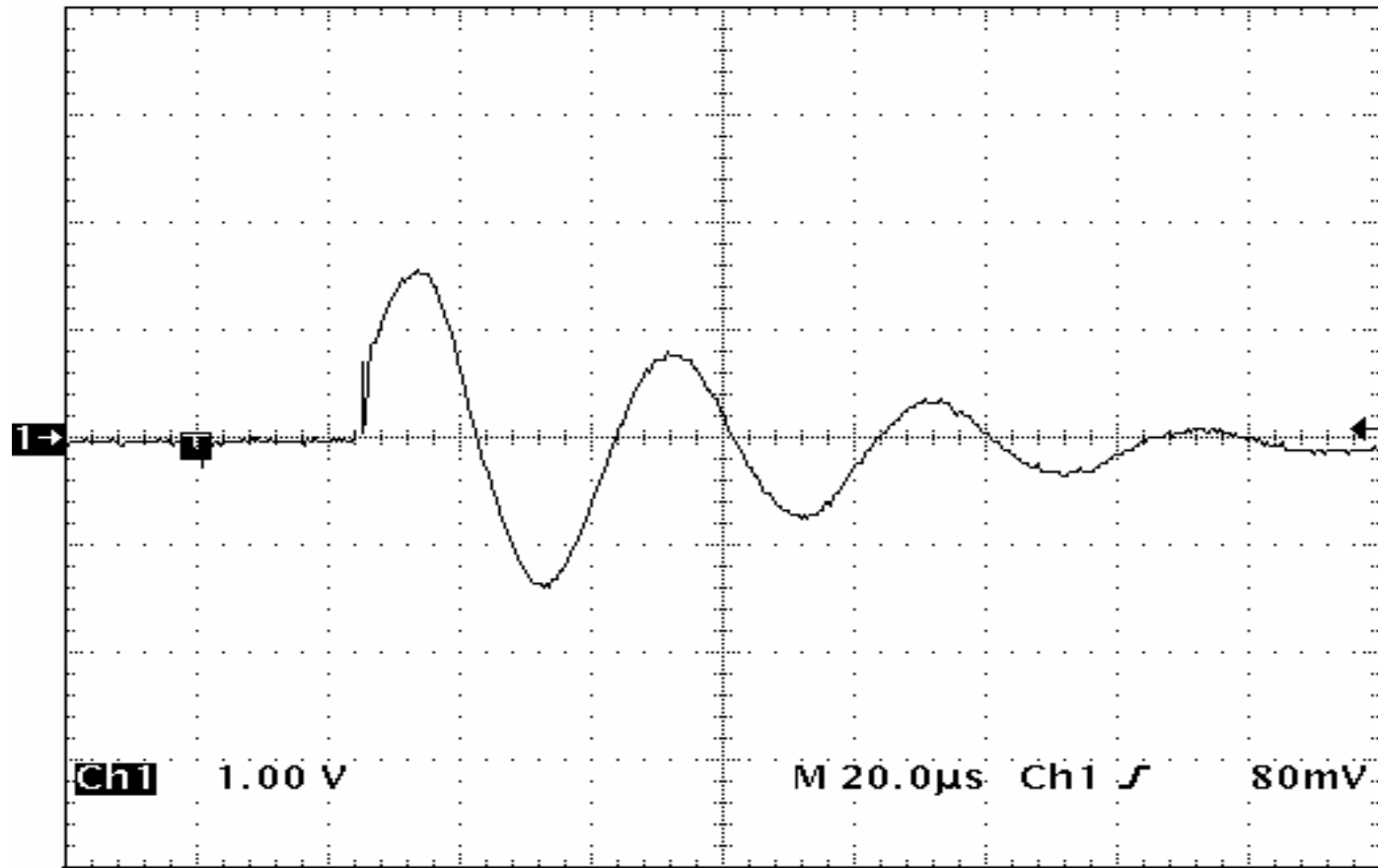
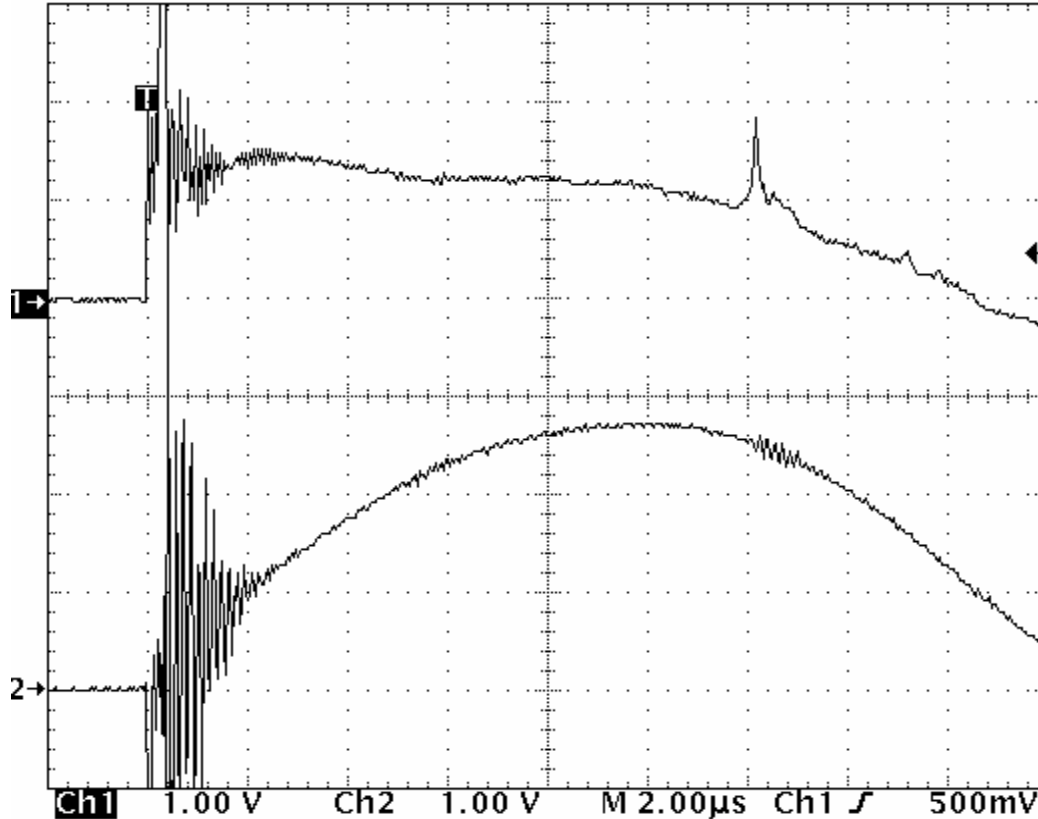
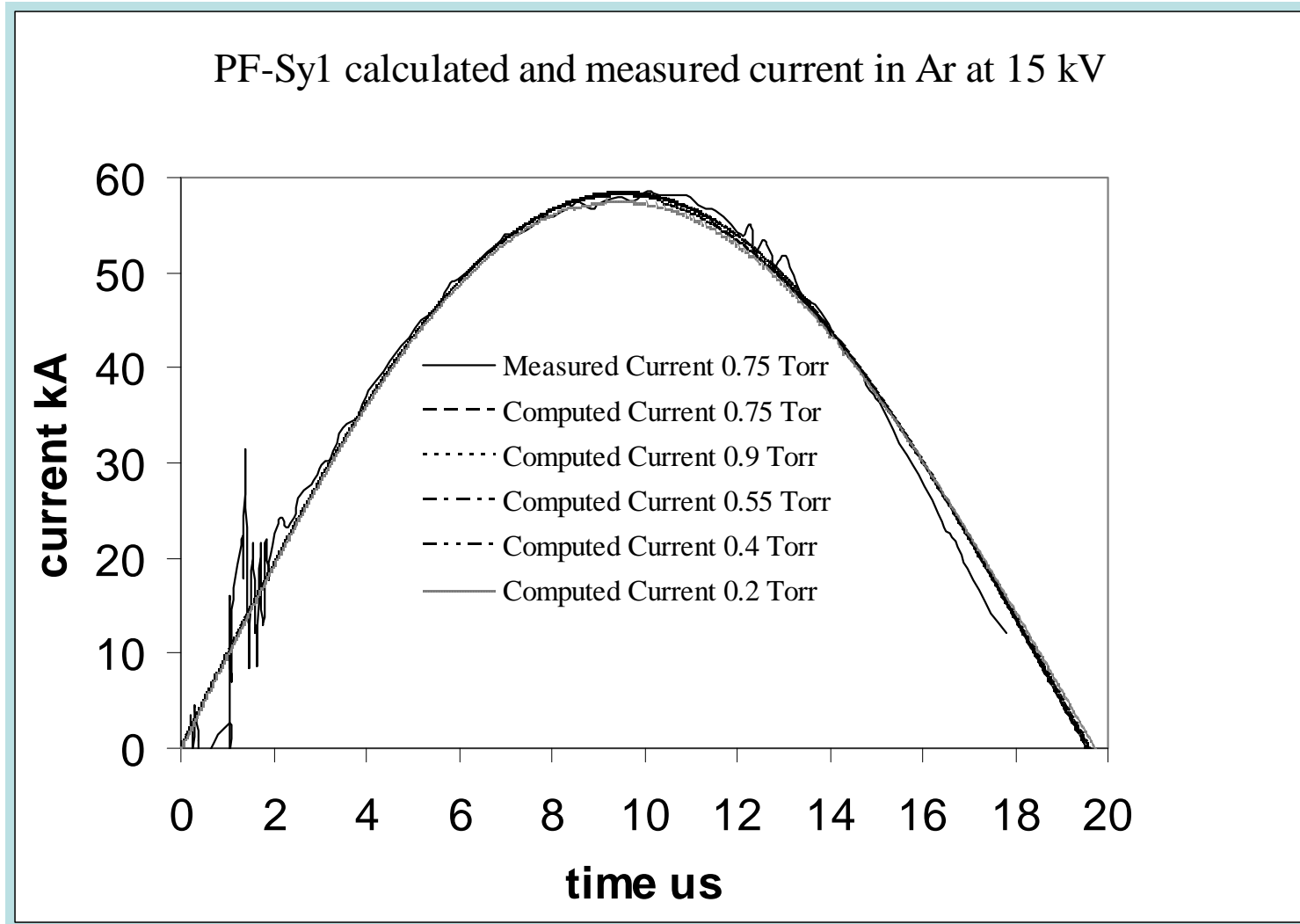


Fig. 2a The measured and calculated current waveform in the case of **L-C-R circuit** of device.

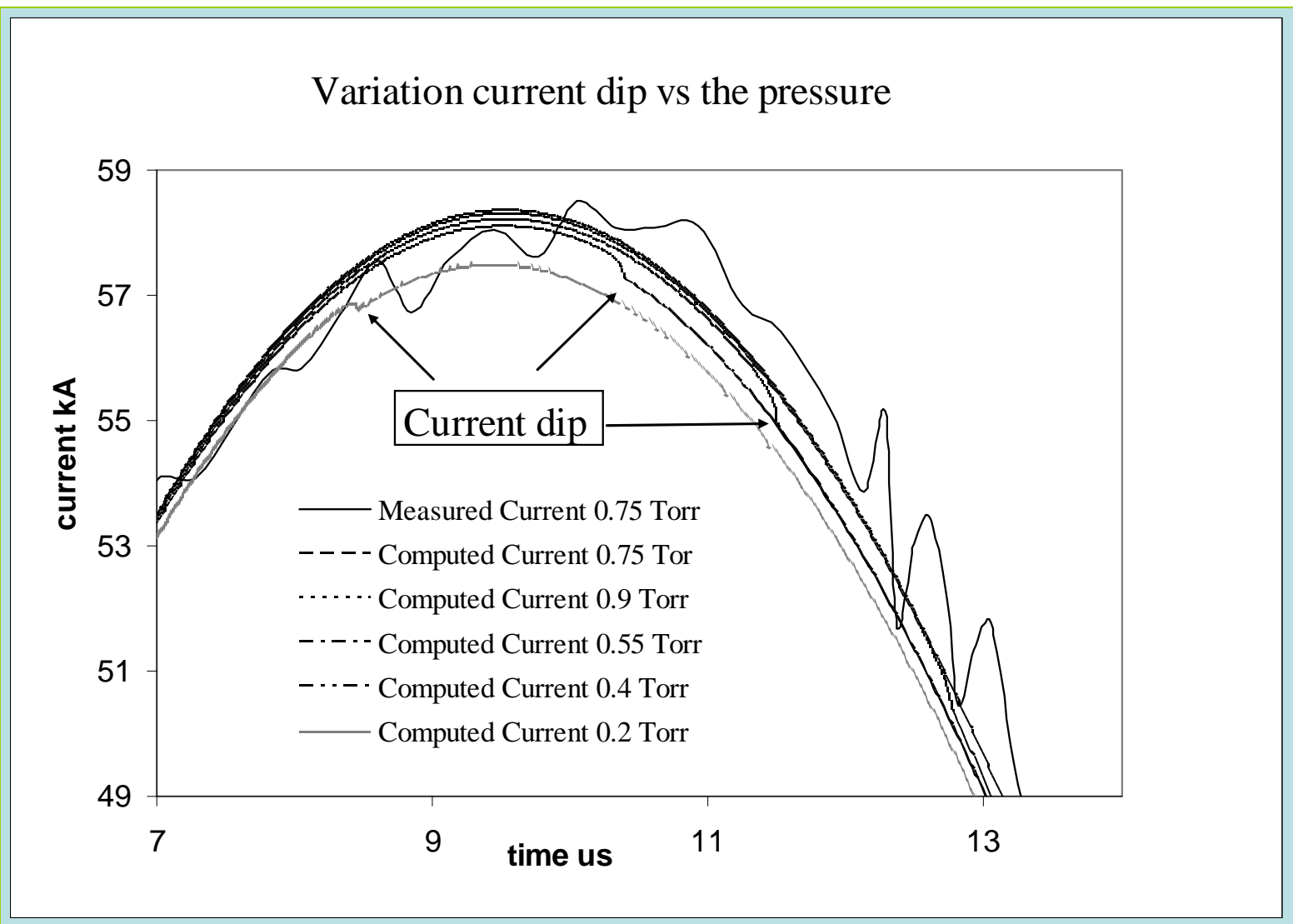




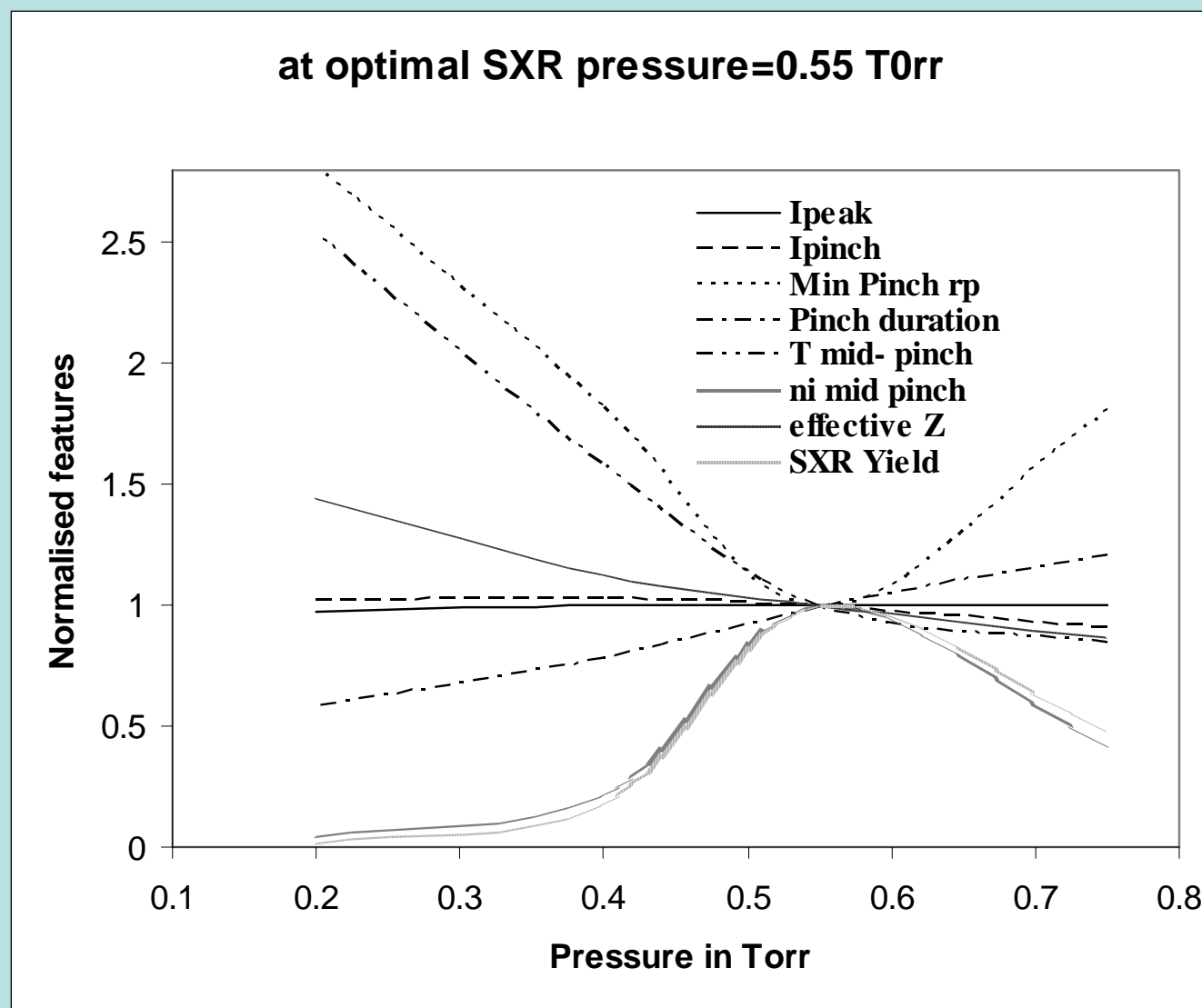
**Fig. 2b** The measured current (down) ( $1\text{V}=21.2\text{ kA}$ ) and voltage (up) ( $1\text{V}=1\text{kV}$ ) waveforms for  $15\text{ kV}$ , and  $0.75\text{ Torr}$  of Ar.



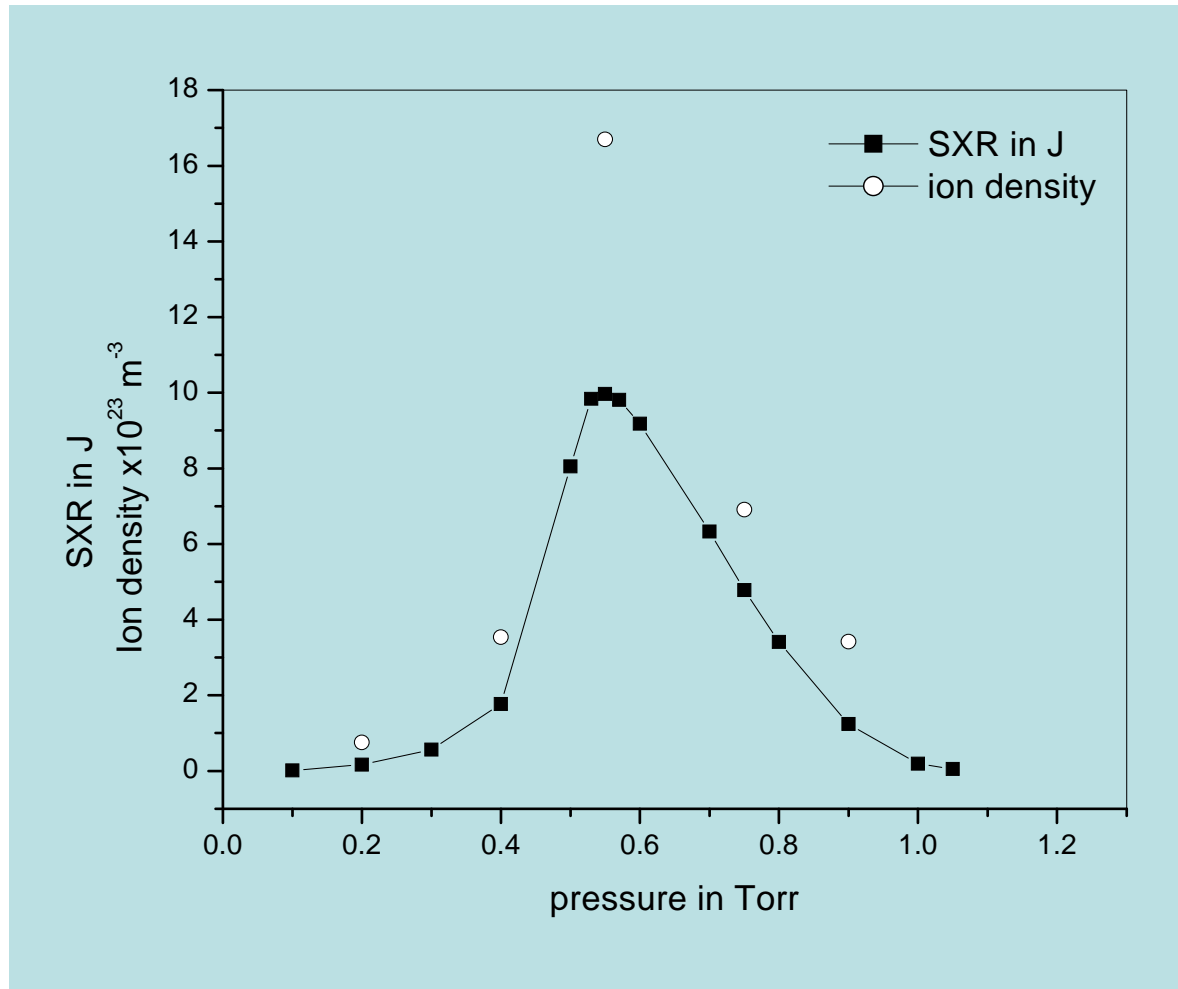
**Fig. 3a** The calculated and measured current – waveforms in Ar at 15 kV for different pressures.



**Fig. 3b** Variation of the current dip on the current – waveforms vs the pressure (enlargement).



**Fig. 4** Normalized characteristic features of PF-Sy1 at optimal case for SXR radiation (**p=0.55 Torr**).



**Fig. 5** Variation of SXR energy as line radiation and ion density vs. the pressure.

$L_0$ , nH	$C_0$ , uF	a, cm	b, cm	$Z_0$ , cm	$r_{0,m}$ Ohm
1525	25	0.95	3.2	16	10
massf	currf	massfr	currfr		
0.1	0.7	0.15	0.7		
$V_0$ , kV	$P_0$ , Torr	MW	A	At-1 mol-2	
15	0.75	40	18	1	

**Tab. I** Given bank , tube, operating parameters and model parameters at 0.75 Torr and applied voltage of 15 kV in Argon (at the best fitting).

$C_0$ uF	$V_0$ kV	$C_0 * V_0$	$3 * T$ us	$T$	$L_0$ nH		$f$	$I_0$ kA	$r_0$ mOhm
25	15	0.375	117.8 5	39.28	1565		0.93 8	85.1	10
	$I_1$	$I_2$	$I_3$	$I_4$	$I_5$	$I_6$			
	57.4	54.8	49.3	47.5	44.12	41.6 8			
	$f_1$	$f_2$	$f_3$	$f_4$	$f_5$				
	0.95 5	0.899	0.963	0.929	0.945				

**Tab. IIa** Calculated characteristic features: period  $T$ , inductance  $L_0$ , resistance  $r_0$ , maximum current  $I_0$  and reversal ratio  $f$  in the case of L-C-R short circuit of device.

$C_0$ uF	$V_0$ kV	$C_0 * V_0$	$3 * T$ us	T	$L_0$ nH		f	$I_0$ kA	$r_0$ mOhm
25	15	0.375	123.7 5	41.2 5	1726		0.813	51.75	34.6
	$I_1$	$I_2$	$I_3$	$I_4$	$I_5$	$I_6$			
	53.85	46.92	25.62	26.9 3	11.54	13.4 8			
	$f_1$	$f_2$	$f_3$	$f_4$	$f_5$				
	0.871	0.546	1.051	0.42 9	1.168				

**Tab. IIb** Measured characteristic features: period **T**, inductance  **$L_0$** , resistance  **$r_0$** , maximum current  **$I_0$**  and reversal ratio **f** in the case of L-C-R circuit (**Ar, 3.75 Torr, 15 kV**).



**Tab. III Comparison of PF-Sy1 characteristics with others PF devices like NX2 (Singapore), PF1000 (Poland), PF400 (Chile) and DPF78 (Germany).**

Plasma focus device	PF-SY1	PF-Sy2	NX2	PF1000	PF400	DPF78
Stored Energy $E_0$ in kJ	2.81	1.5	1.7	486	0.37	30.96
Pressure in Torr, $P_0$	0.55	0.54	2.9	3.5	6.6	7.5
Anode radius a in cm	0.95	0.95	1.9	11.55	0.6	2.5
c=b/a	3.37	3.37	2.16	1.39	2.6	2
anode length $z_0$ in cm	16	16	5	60	1.7	13.7
final pinch radius $r_{\min}$ in cm	0.023	0.0235	0.172	2.3	0.086	0.372
pinch length $z_{\max}$ in cm	1.74	1.71	2.79	18.9	0.85	3.66
pinch duration in ns	14.532	14.709	30.6	282	5.3	21.276
$r_{\min}/a$	0.024	0.025	0.091	0.2	0.143	0.1488
$z_{\max}/a$	1.83	1.8	1.47	1.64	1.42	1.464
$I_{\text{peak}}$ in kA	58.2	82.5	369.4	1845	126	867.6

<b>I<sub>peak</sub>/a in kA/cm</b>	<b>61.26</b>	<b>86.84</b>	<b>194.42</b>	<b>160</b>	<b>210</b>	<b>347.04</b>
<b>S=(I<sub>peak</sub>/a)/(P<sub>o</sub><sup>1/2</sup>)( kA/cm)/Torr<sup>1/2</sup></b>	<b>82.61</b>	<b>118.177</b>	<b>114</b>	<b>85.6</b>	<b>81.7</b>	<b>126.7</b>
<b>I<sub>pinch</sub> in kA</b>	<b>38.6</b>	<b>38.9</b>	<b>142</b>	<b>784</b>	<b>81.3</b>	<b>437.4</b>
<b>I<sub>pinch</sub>/I<sub>peak</sub></b>	<b>0.66</b>	<b>0.47</b>	<b>0.38</b>	<b>0.425</b>	<b>0.65</b>	<b>0.504</b>
<b>Peak induced voltage in kV</b>	<b>33.4</b>	<b>32.3</b>	<b>20.3</b>	<b>40.1</b>	<b>16.7</b>	<b>79.2</b>
<b>peak axial speed in cm/us</b>	<b>2.19</b>	<b>3.37</b>	<b>5.8</b>	<b>11.2</b>	<b>9</b>	<b>15.7</b>
<b>peak radial shock speed cm/us</b>	<b>13</b>	<b>13.4</b>	<b>20.6</b>	<b>16.4</b>	<b>34.3</b>	<b>-36.2</b>
<b>peak radial piston speed cm/us</b>	<b>6.91</b>	<b>11.3</b>	<b>14.5</b>	<b>10.9</b>	<b>22.9</b>	<b>-24.2</b>
<b>peak temperature in 10<sup>6</sup>K</b>	<b>1.59</b>	<b>1.79</b>	<b>1.52</b>	<b>1.14</b>	<b>6.1</b>	<b>6.58</b>
<b>SXY yield in J</b>	<b>9.97</b>	<b>9.31</b>	<b>20.8</b>	<b>-</b>	<b>-</b>	<b>-</b>

# Conclusion

In this work we have applied RADV5.13.9b program to fit a computed current trace with a measured waveform varying the model parameters, given all bank, tube and operating parameters, in addition to that the current waveform was calculated at different pressures.

The parameters such as  $L_0$  ,  $I_0$  and  $r_0$  were determined from the measured and calculated current waveform and compared between them.

- **It was shown also the variation of normalized main properties of the plasma like  $I_{peak}$ ,  $I_{pinch}$ , temperature and SXR yield and others vs. the pressure in related to the case of optimal SXR and the variation of SXR and ion density according to the pressure.**
- **The calculations have allowed comparing our PF device characteristics with other small and big PF devices.**

# References

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**Thank You**